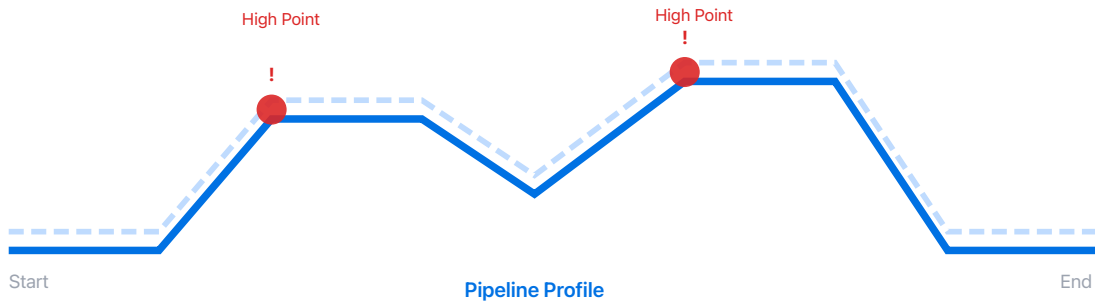


ENGINEERING CHECKLIST — PRESSURE PIPELINES

10 Common Mistakes in Pressure Pipeline Design

A practical guide for water infrastructure engineers — covering the most critical design errors that lead to pipeline failures, cost overruns, and safety hazards.



- | | |
|---|--|
| 1 Column Separation at High Points | 2 Pipe Diameter Selection by Velocity Only |
| 3 Neglecting Air Valves at High Points | 4 Transient Pressure at Startup |
| 5 Thermal Expansion in Above-Ground Pipes | 6 Manual Calculations vs. Hydraulic Simulation |
| 7 Incorrect Isolation Valve Placement | 8 Thrust Forces at Bends & Fittings |
| 9 Pre-charge Pressure for Surge Vessels | 10 No Network Testing Before Commissioning |

CRITICAL DESIGN ERROR

Ignoring Column Separation at Pipeline High Points

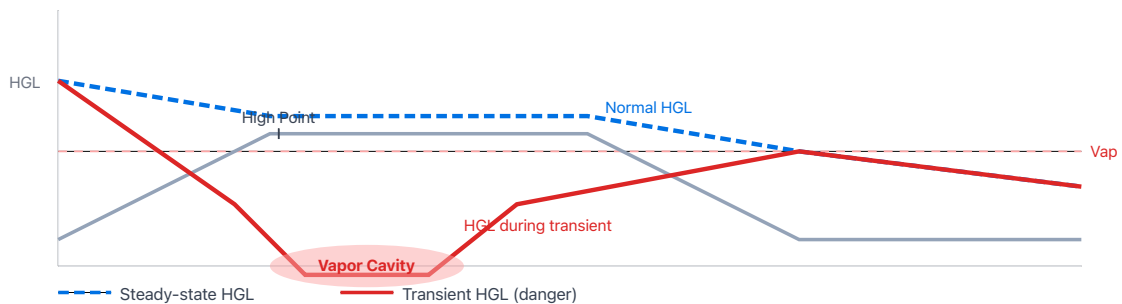
WHY IT HAPPENS

Engineers focus on protecting pipelines from positive pressure surges (water hammer) but overlook negative pressure events. When flow decelerates suddenly, pressure at high points can drop below the liquid's vapor pressure — causing the water column to separate and a vapor cavity to form. When this cavity collapses, it generates a violent pressure shock far exceeding the initial water hammer.

THE RISK

- ▲ Catastrophic pipe rupture upon cavity collapse
- ▲ Pressure spikes 3–5x higher than standard water hammer
- ▲ Pipe deformation and permanent structural damage
- ▲ Complete system shutdown and costly emergency repairs
- ▲ Serious safety hazard to field personnel

HYDRAULIC GRADE LINE — COLUMN SEPARATION AT HIGH POINT



THE RIGHT APPROACH

- | | |
|--|--|
| <p>1 Run full hydraulic transient analysis including negative pressure scenarios at all high points</p> | <p>2 Install Combination Air Valves at all high points to prevent sub-atmospheric pressure</p> |
| <p>3 Consider surge vessels or flywheels to slow down pump deceleration during power failure</p> | <p>4 Verify that pipe pressure rating accounts for both positive and negative transient pressures</p> |

ECONOMIC & HYDRAULIC ERROR

Selecting Pipe Diameter Based on Flow Velocity Alone

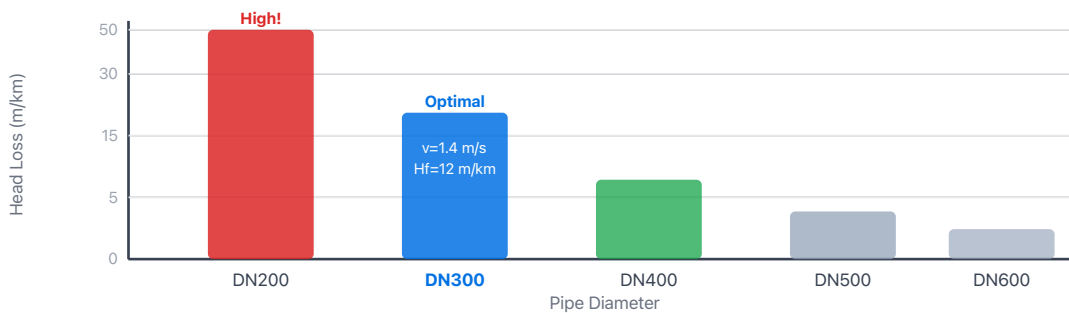
WHY IT HAPPENS

Many engineers apply a simple rule of thumb — keep velocity between 0.5 and 2.0 m/s — and stop there. This ignores head loss, energy consumption, capital cost trade-offs, and the pipeline's full operational life. A pipe that meets the velocity criterion may still be economically and hydraulically suboptimal, leading to either undersized or oversized designs.

THE RISK

- ▲ Oversized pipes: unnecessary capital cost & slow velocities causing sedimentation
- ▲ Undersized pipes: excessive head loss, high energy bills over 20–30 year lifespan
- ▲ Incorrect pump selection based on wrong system curve
- ▲ Inability to handle future demand growth
- ▲ Increased water hammer risk in undersized pipes

HEAD LOSS VS. PIPE DIAMETER — SAME FLOW RATE (Q = 100 L/S)



THE RIGHT APPROACH

- 1 Perform a **life-cycle cost analysis** combining capital cost, energy, and maintenance over 25+ years
- 2 Use the **Hazen-Williams or Darcy-Weisbach** equation to calculate head loss for candidate diameters
- 3 Check velocity against **sedimentation limits (min 0.6 m/s)** and erosion limits (max 3 m/s for steel)
- 4 Account for **future demand growth** — size the pipe for the 20-year projected flow, not today's flow

CRITICAL INSTALLATION ERROR

Neglecting Air Valves at Pipeline High Points

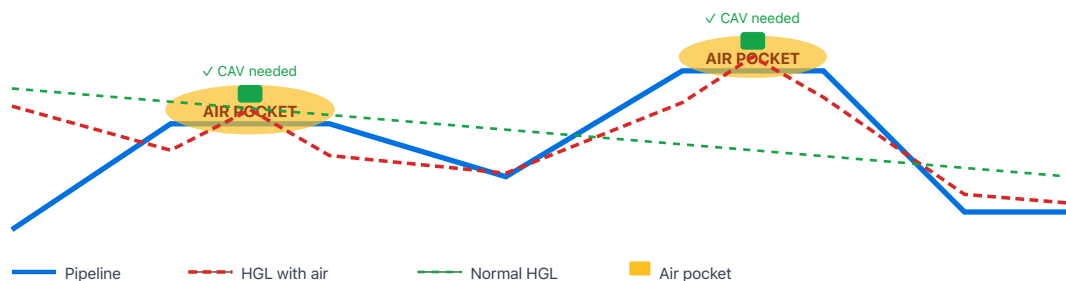
WHY IT HAPPENS

Engineers design the hydraulic profile but fail to systematically identify every local high point along the alignment. Air valves are often treated as optional accessories rather than critical protection devices. In some cases, valves are omitted to reduce cost — without understanding that trapped air pockets dramatically reduce hydraulic capacity and can trigger column separation and pipeline collapse.

THE RISK

- ▲ Air pockets reduce effective pipe cross-section and flow capacity by up to 40%
- ▲ Trapped air triggers column separation and violent pressure surges
- ▲ Air locks prevent pipeline from reaching full operation
- ▲ Negative pressures during draining can cause pipe collapse
- ▲ Uncontrolled air release causes destructive pressure spikes

PIPELINE PROFILE — AIR ACCUMULATION WITHOUT AIR VALVES



THE RIGHT APPROACH

- 1 Plot the full pipeline profile and **identify every local high point** — even minor ones in flat terrain
- 2 Install **Combination Air Valves (CAV)** at each high point — they handle air intake, release, and vacuum breaking
- 3 Size air valves properly using **inlet/outlet flow rates** — an undersized valve can be worse than none
- 4 Ensure **controlled filling and draining procedures** that allow gradual air displacement through valves

CRITICAL DESIGN ERROR

Failure to Account for Transient Pressure at Startup

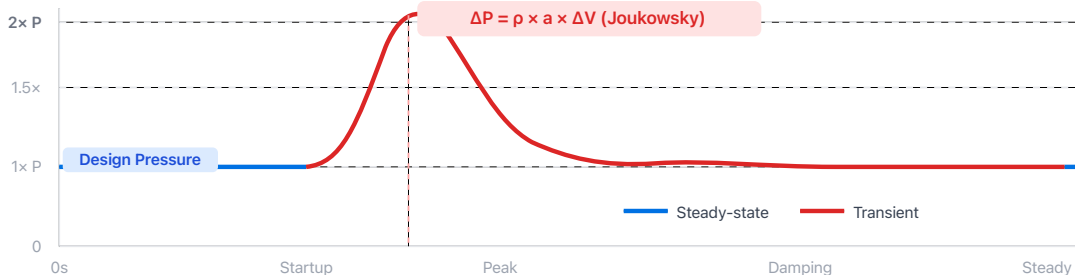
WHY IT HAPPENS

Engineers design pipelines based on **static pressure only**, ignoring that sudden pump startup or valve closure generates transient pressure spikes that can far exceed the pipe's design pressure. This is often due to over-reliance on steady-state calculations and skipping dynamic hydraulic simulation entirely.

THE RISK

- ▲ Pipe bursting or cracking at very first operation
- ▲ Irreversible pump and valve damage
- ▲ Major financial losses and project delays
- ▲ Safety hazards for commissioning personnel
- ▲ Costly retrofitting of surge protection after construction

PRESSURE VS. TIME — TRANSIENT SPIKE AT PUMP STARTUP



THE RIGHT APPROACH

- 1 Calculate transient pressure using the **Joukowsky equation** as a minimum baseline check
- 2 Run **hydraulic transient simulation** for all operating scenarios including power failure
- 3 Design **surge protection before construction** — not as an afterthought during commissioning
- 4 Consider **surge vessels, PRVs**, and controlled valve closure times as protection measures

STRUCTURAL DESIGN ERROR

Ignoring Thermal Expansion in Above-Ground Pipelines

WHY IT HAPPENS

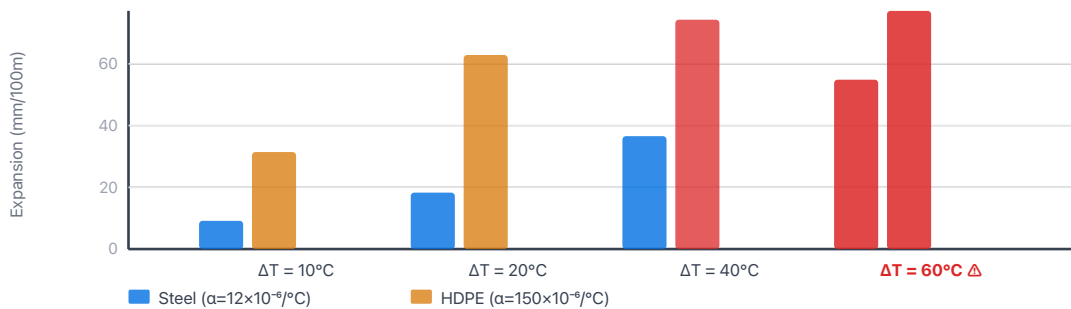
Engineers correctly apply thermal expansion calculations for process piping but often neglect them in water infrastructure projects. Above-ground pipelines in hot climates (like Saudi Arabia) experience temperature swings of 40–60°C, causing significant longitudinal expansion. When pipe movement is restrained by fixed supports, enormous axial forces develop — leading to structural failure of joints, supports, or the pipe itself.

$$\Delta L = \alpha \times L \times \Delta T$$

THE RISK

- ▲ Flange joint separation and leaks at pipe connections
- ▲ Support bracket failure under repeated thermal cycling
- ▲ Pipe buckling in sections with insufficient expansion loops
- ▲ Gasket degradation and premature seal failure
- ▲ Fatigue cracking at fixed anchor points over time

THERMAL EXPANSION (MM/100M) VS. TEMPERATURE RISE — COMMON PIPE MATERIALS



THE RIGHT APPROACH

- 1 Calculate thermal expansion using $\Delta L = \alpha \times L \times \Delta T$ for each pipe segment and material
- 2 Install **expansion joints or expansion loops** at calculated intervals to absorb movement
- 3 Use **guided and anchored supports** correctly — distinguish between fixed anchors and sliding supports
- 4 Use site-specific temperature data — in hot climates, design for **ΔT up to 60°C**, not standard values

METHODOLOGY ERROR

Relying on Manual Calculations Instead of Hydraulic Simulation

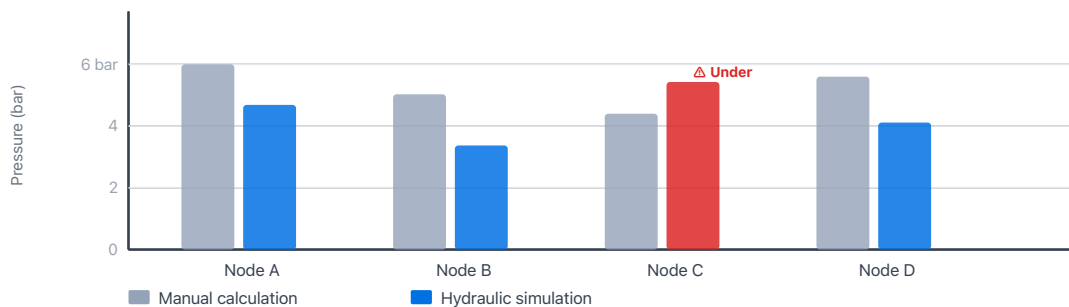
WHY IT HAPPENS

Manual calculations work well for simple, single-pipe systems. However, when applied to complex looped networks, multiple pump configurations, or transient scenarios, they cannot capture the interaction between system components. Engineers often trust spreadsheets built on steady-state assumptions, missing dynamic behaviors that only emerge during simulation — leading to designs that fail under real operating conditions.

THE RISK

- ▲ Missing critical surge and transient scenarios entirely
- ▲ Incorrect pump operating point — pump runs in unstable zone
- ▲ Underestimating head loss in looped networks
- ▲ Oversized or undersized surge protection equipment
- ▲ Expensive re-engineering after commissioning failures

MANUAL CALCULATION VS. HYDRAULIC SIMULATION — PRESSURE RESULTS COMPARISON



THE RIGHT APPROACH

- 1 Use hydraulic modeling software such as **EPANET, Bentley WaterGEMS, or InfoWorks WS** for all network analysis
- 2 Model **all operating scenarios**: peak demand, minimum flow, pump failure, and emergency conditions
- 3 Run **transient (dynamic) simulation** separately from steady-state — they answer different questions
- 4 **Validate the model** against field measurements before using results for final design decisions

OPERATIONS & MAINTENANCE ERROR

Incorrect Placement of Isolation Valves

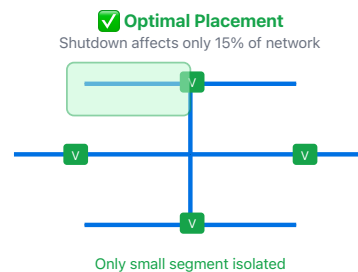
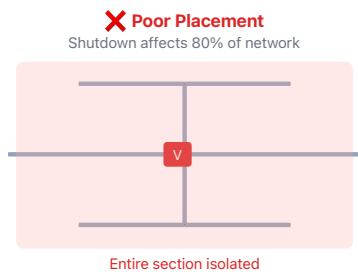
WHY IT HAPPENS

Isolation valves are placed at convenient locations during design — at road crossings, at accessible chambers — rather than at strategic positions based on operational and maintenance analysis. Engineers often minimize valve count to cut costs, without evaluating how large a section of the network must be shut down when a single valve closes. The result is a system that cannot be maintained without major service interruptions.

THE RISK

- ▲ Large network sections shut down for minor repairs — affecting thousands of users
- ▲ Inability to isolate a failure quickly, extending damage and downtime
- ▲ No flexibility to redirect flow during emergencies
- ▲ Higher repair costs due to uncontrolled water loss before isolation
- ▲ Regulatory non-compliance in critical water supply systems

NETWORK ISOLATION COVERAGE — POOR VS. OPTIMAL VALVE PLACEMENT



THE RIGHT APPROACH

- 1 Apply the **N-1 rule**: closing any single valve should isolate the minimum possible network segment
- 2 Map all **critical nodes and users** first, then work backwards to determine optimal valve positions
- 3 Evaluate valve placement based on **maintenance frequency** — high-risk segments need closer valve spacing
- 4 Document a **valve operation plan** for each maintenance and emergency scenario before design approval

STRUCTURAL SAFETY ERROR

Neglecting Thrust Forces at Pipe Bends and Fittings

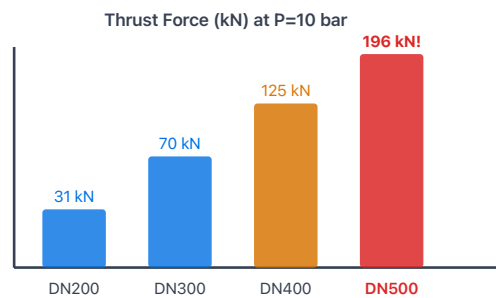
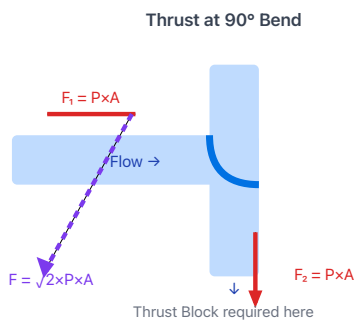
WHY IT HAPPENS

Designers correctly size the pipe for flow and pressure, but fail to calculate the unbalanced hydrostatic thrust forces that act at every bend, tee, reducer, and end cap. These forces — often several tonnes — must be resisted by thrust blocks or restrained joints. When omitted, the first pressure test or transient event causes joint separation. This mistake is especially common when design is done without reference to the installed soil conditions.

THE RISK

- ▲ Joint blow-out during first hydrostatic pressure test
- ▲ Pipe movement and misalignment at unrestrained fittings
- ▲ Catastrophic failure and flooding at commissioning
- ▲ Undermining of adjacent structures and roads
- ▲ Complete re-excavation and re-installation of affected sections

THRUST FORCE AT 90° BEND — FORCE DIAGRAM & MAGNITUDE VS. PIPE SIZE



THE RIGHT APPROACH

1 Calculate thrust forces at **all bends, tees, reducers, and end caps** using $F = P \times A \times 2\sin(\theta/2)$

2 Design **concrete thrust blocks** sized for local soil bearing capacity and the calculated thrust force

3 Consider **restrained joint systems** as an alternative to thrust blocks — more reliable in poor soils

4 Always verify thrust block design before **hydrostatic pressure testing** — test pressure amplifies forces

SURGE PROTECTION ERROR

Incorrect Pre-charge Pressure for Surge Vessels

WHY IT HAPPENS

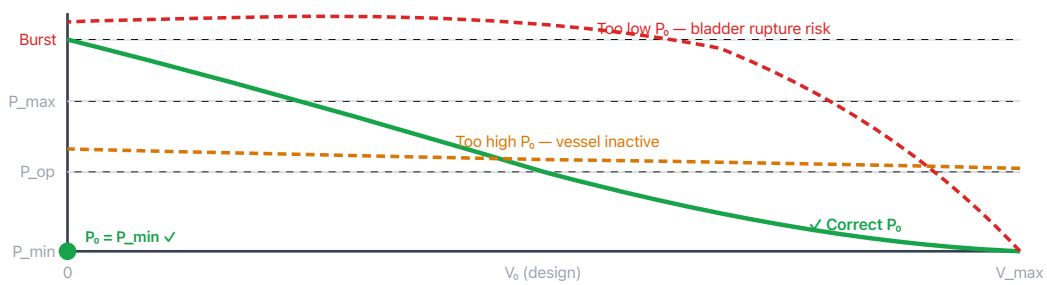
Engineers correctly specify a surge vessel (hydropneumatic tank) for surge protection but set the initial air pre-charge pressure incorrectly. Some use the pump shutoff pressure; others use a fixed value from a reference project. The pre-charge pressure must equal the **minimum steady-state pressure at the vessel location** — any deviation makes the vessel either ineffective or counterproductive, leaving the pipeline completely unprotected during transient events.

$$P_0 = P_{\min} \text{ at vessel location}$$

THE RISK

- ▲ Too high pre-charge: vessel never activates — pipeline unprotected
- ▲ Too low pre-charge: vessel loses all air rapidly — becomes a dead water tank
- ▲ Bladder rupture due to over-compression from wrong pre-charge
- ▲ False confidence — vessel is installed but provides zero protection
- ▲ Pipeline failure during first pump trip event

SURGE VESSEL: PRESSURE VS. VOLUME — CORRECT VS. INCORRECT PRE-CHARGE



THE RIGHT APPROACH

- | | |
|---|--|
| <p>1 Set pre-charge pressure equal to minimum steady-state pressure at the vessel location — not at the pump</p> | <p>2 Verify the pre-charge setting using transient simulation to confirm the vessel activates correctly</p> |
| <p>3 Check pre-charge pressure periodically</p> | <p>4 Size the vessel volume based on worst-case</p> |

during operation — air leaks through the bladder over time

transient scenario — pump trip under maximum flow

COMMISSIONING ERROR

Skipping Network Testing Before Commissioning

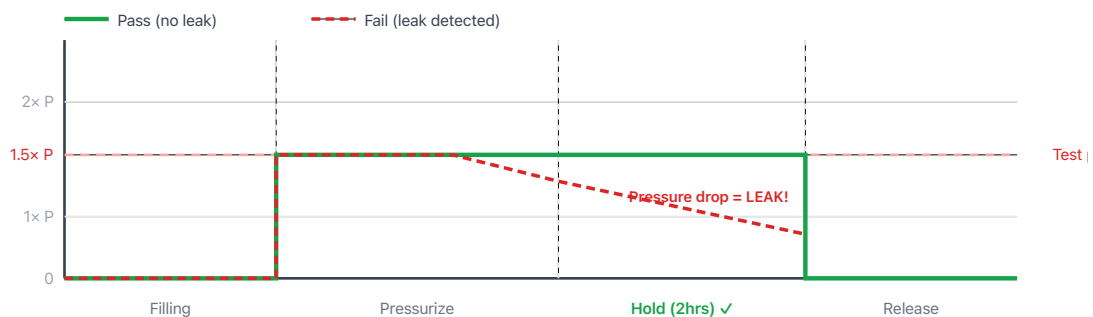
WHY IT HAPPENS

Schedule pressure and budget constraints push project teams to skip or shorten proper commissioning procedures. Hydrostatic pressure testing, pipeline flushing, and gradual startup protocols are seen as "delays" rather than essential quality gates. This is especially common when the contractor controls commissioning without proper engineering oversight — leading to operational failures that are far more expensive than the testing that was omitted.

THE RISK

- ▲ Undetected leaks cause ground subsidence and structural damage
- ▲ Air pockets trapped in system reduce capacity and cause pressure surges
- ▲ Contamination of water supply reaching end users
- ▲ Pump cavitation from air-filled pipelines on first start
- ▲ Premature failure of joints, valves, and instruments

HYDROSTATIC PRESSURE TEST PROTOCOL — PRESSURE VS. TIME



THE RIGHT APPROACH

- 1 Perform **hydrostatic pressure test at 1.5x operating pressure** held for minimum 2 hours with zero drop
- 2 Flush the pipeline at high velocity (**min 1.5 m/s**) to remove debris, sediment, and air pockets
- 3 Follow a **slow, controlled startup sequence** — never open isolation valves fully in one operation
- 4 For potable water: perform **chlorination and bacteriological testing** before any connection to supply

